

Hochschule Karlsruhe

University of
Applied Sciences

Institut für
Energieeffiziente Mobilität

Approach to a Holistic Modelling of Cycling Dynamics

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Education and Experience:

- Master's Degree in Automotive Systems Engineering
from Karlsruhe University of Applied Sciences
- Research Assistant at Institute of Energy Efficient Mobility

Research Interests:

- Modelling and Simulation of Cycling
- Energy Management Systems for Electric Vehicles
- Energy Prediction and Management for E-Bikes/Pedelecs

Motivation and Use-Cases



Promoting Cycling as Part of New Mobility Strategies

Potential Use-Cases:

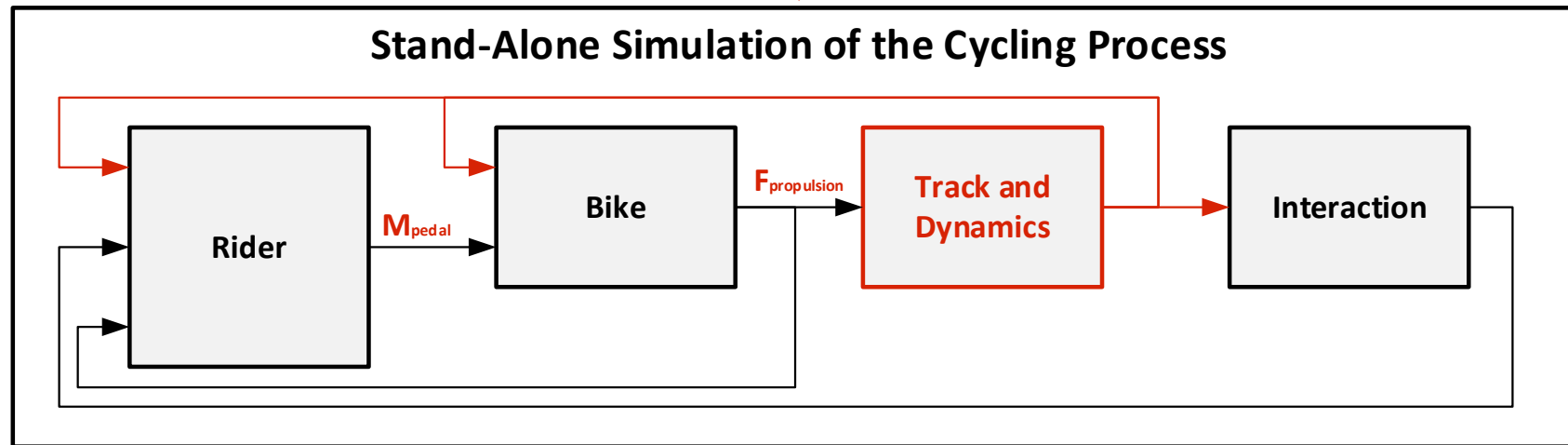
A-priori simulation based quality evaluation of cycling infrastructure
→ Focusing on physical aspects with relevance to the cyclist

Usage of Model-Based Methods

(Increased) Technologicalisation of Cycling → E-Bikes/Pedelcs

Potential Use-Cases:

- model-based development of components or functions
- increased energy demand prediction for E-Bikes



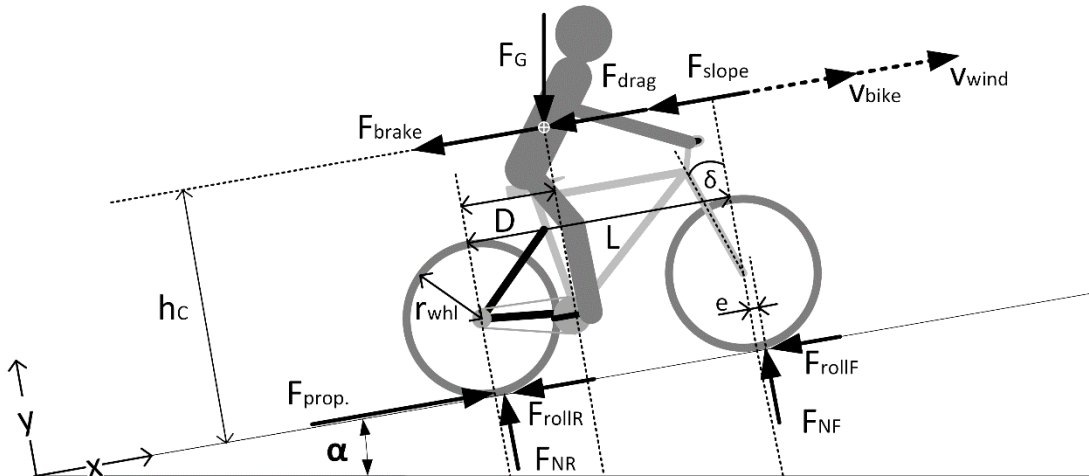
➔ Resulting dynamics define the physical model structure of bike and rider subsystems

Modelling Cycling Dynamics

Longitudinal Dynamics

Given as a-priori knowledge:

- trajectory of the cycled path
- further route properties (e.g. slope, wind)



Description of Longitudinal Dynamics:

$$m a = F_{prop.} - F_{brake} - F_{roll} - F_{slope} - F_{drag}$$

$$v(t) = \int a(t) dt$$

Slope Resistance:

$$F_{slope} = F_G \sin(\alpha) = m g \sin(\alpha)$$

Drag Resistance:

$$F_{drag} = \frac{1}{2} \rho_{air} c_W A (v_{bike} - v_{wind})^2$$

Roll Resistance:

$$F_{roll} = F_N f_R = F_G \cos(\alpha) f_R = m g \cos(\alpha) f_R$$

(f_R representing tyre flexing-, roll off- and surface-resistance)

Transient Resistance:

Longitudinal and rotational inertia represented in

Resulting Dynamics description:

$$\lambda m a = F_{prop.} - F_{brake} - F_{roll} - F_{slope} - F_{drag}$$



Modelling Cycling Dynamics

Lateral Dynamics – Bicycle Balance



Modelling Conditions and Assumptions:

- given trajectory of the cycled path
➔ given steering curve radius (r_c)
- stability of the bicycle is given
- ideal curve is assumed

Representing the tilt angle (γ) of the bicycle caused by deflection of the centre of gravity in relation to the point of contact:

- determination by ratio between centrifugal (F_C) and normal force (F_N):

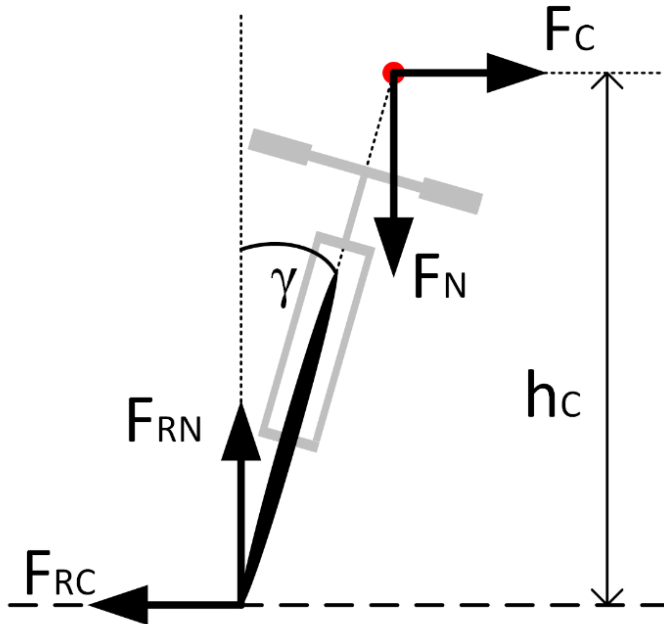
$$F_C = \frac{m v^2}{r_c}$$

- **condition for stable cornering:**
generation of equal torque by normal and centrifugal force

$$F_G h_c \sin(\gamma) = \frac{m v^2}{r_c} h_c \cos(\gamma)$$

Resulting tilt angle:

$$\tan(\gamma) = \frac{v^2}{g r_c}$$

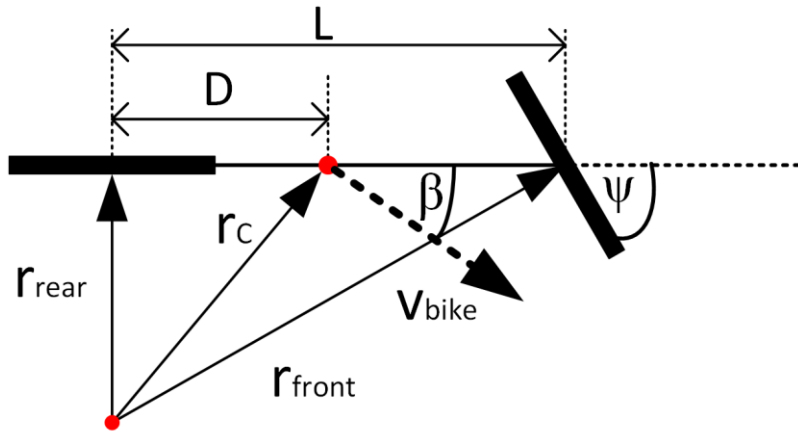


Modelling Cycling Dynamics

Lateral Dynamics – Bicycle Steering

Modelling Conditions and Assumptions:

- given trajectory of the cycled path
 - ➔ given steering curve radius (r_c)
- ideal curve is assumed



Calculating the turn angle (θ) of the handlebar:

- calculating yaw angle (β) around the centre of gravity

$$\sin(\beta) = \frac{D}{r_c}$$

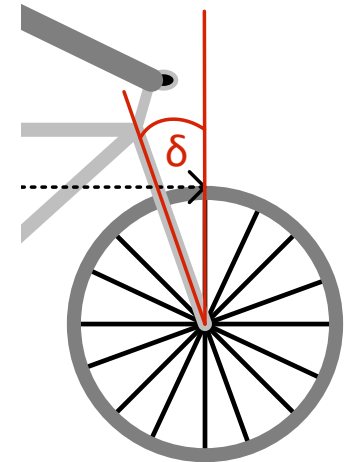
- calculating front wheel angle (ψ)

$$\tan(\psi) = \frac{L}{D} \tan(\beta)$$

Calculating turn angle of the handlebar (θ)

(assuming a small head tube angle (δ))

$$\tan(\theta) = \frac{\psi}{\sin(\delta)}$$



Modelling Cycling Dynamics

Braking Dynamics

Dynamic limitations of cycling occur primarily during braking

Fairly low propulsion force doesn't cause spinning wheels

Intensive braking quickly exceeds friction limits

→ *wheel lock up*

Calculating maximum braking force using static friction force:

$$F_{B_{max}} = F_S = \mu_s F_N = \mu_s m g \cos(\alpha)$$

Considering static and dynamic normal force distribution:

$$F_{N_{front}} = \frac{F_N D - m a h_s}{L} \text{ and } F_{N_{rear}} = \frac{F_N (L - D) - m a h_s}{L}$$

→ **different maximum braking force on front and rear wheel**

Braking in Curve Situations:

- maximum braking force is decreased
- static friction also used for lateral traction

$$\rightarrow F_{B_{max}} = \sqrt{F_S^2 - F_C^2}$$

centrifugal force used as lateral guidance force

Calculating resulting centrifugal force on front and rear wheel:

considering speed, curve radius and weight distribution

$$F_{C_{front}} = \frac{m D v^2}{L \sqrt{r_c^2 - D^2 + L^2}} \text{ and } F_{C_{rear}} = \frac{m (L - D) v^2}{L \sqrt{r_c^2 - D^2}}$$



Implementation

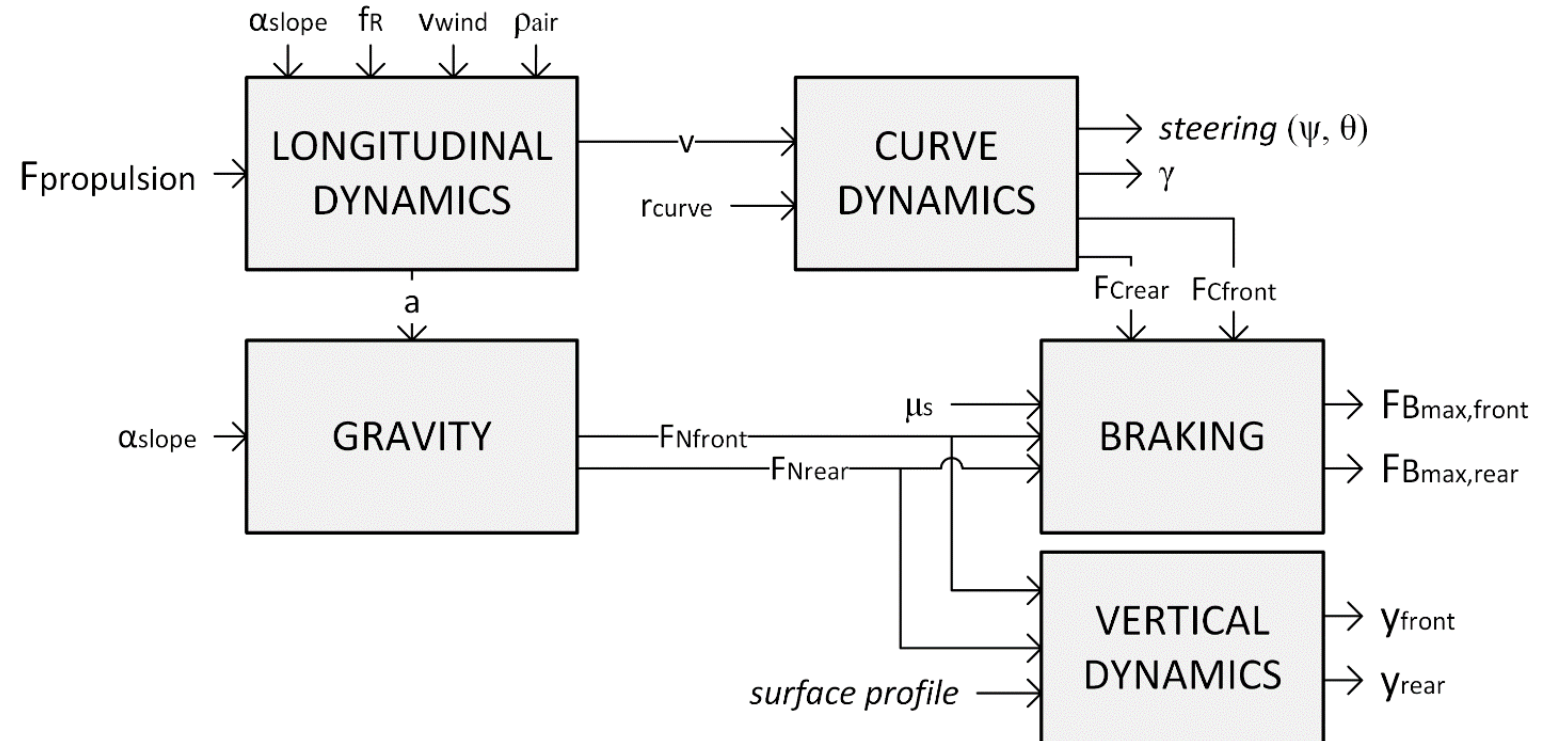
Resulting Model



Physical equations derived by the dynamics description of cycling implemented in MATLAB/Simulink

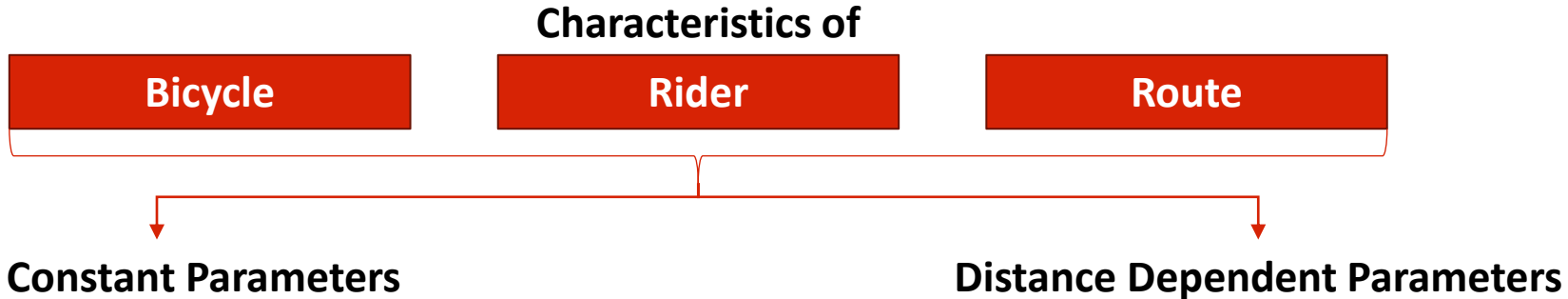
Generated a-priori knowledge by pre-processing:

- α_{slope} : slope angle
- f_R : roll resistance factor
- v_{wind} : wind speed
- ρ_{air} : air density
- r_{Curve} : curve radius
- μ_s : static friction coefficient
- surface profile



Implementation

Modelling Parameters



For generic bicycles: rule-based derivation of parameters

- in dependence of the bicycle type and rider's physique:

c_W -Value, frontal Area, centre of gravity position

- in dependence of the bicycle type:

head tube angle, wheelbase, spring-damper-parameters

- in dependence of the tyre type:

vertical dynamic tyre properties

For specific bicycles:

- technical documentation
- experimental determination, e.g. coasting experiment

Synthetic routes:

Required to self define all properties

Routes based on real infrastructure:

Self-developed route data generation algorithm, enables calculation of:

- *curve radius* based on route trajectory
- *slope angle* based on altitude
- *air density* based on altitude, air pressure, humidity and temperature
- *resulting wind speed* based on wind speed and direction
- *rolling resistance factor* and *static friction coefficient* based on underground as well as tyre type and pressure

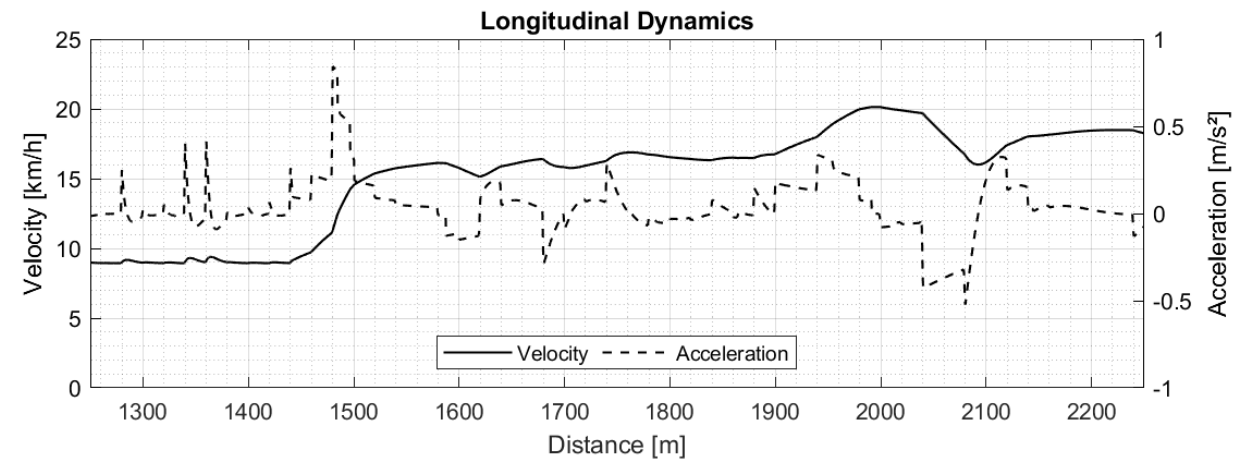
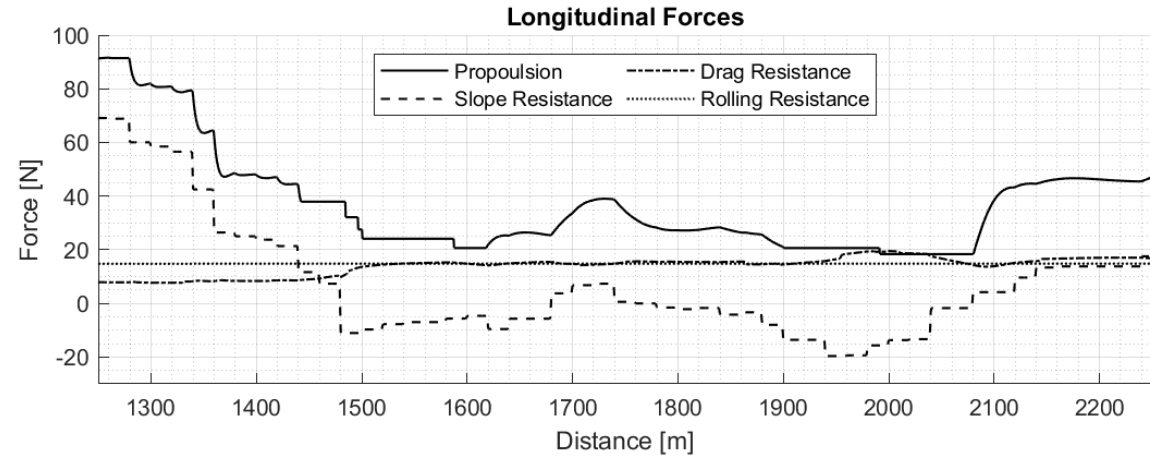
Simulation and Results

Longitudinal Dynamics



Simulation of cycling on a forest road

- starting with an uphill section → significant slope resistance results in lower speed ✓
- end of uphill section → increased speed ✓
- increased velocity → drag resistance ✓
- constant rolling resistance → due to no change of underground ✓

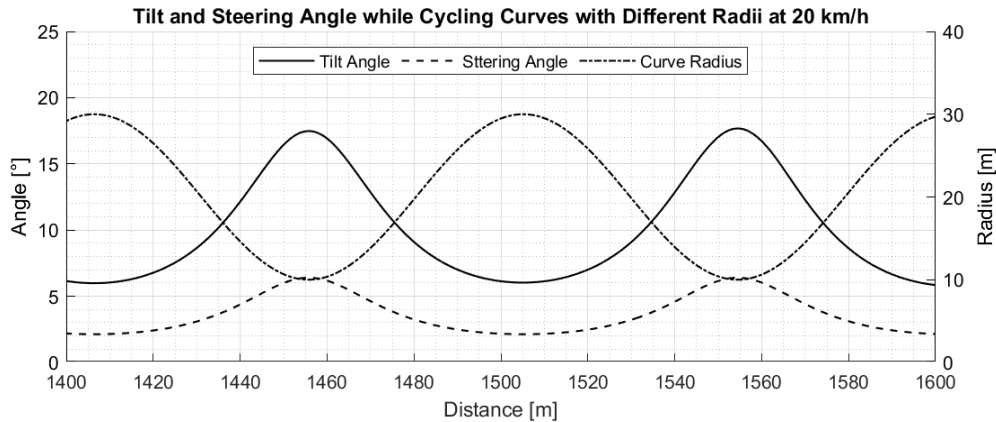


Simulation and Results

Lateral and Braking Dynamics



Periodically cycling curve radius between 10 to 30 meters at 20 km/h

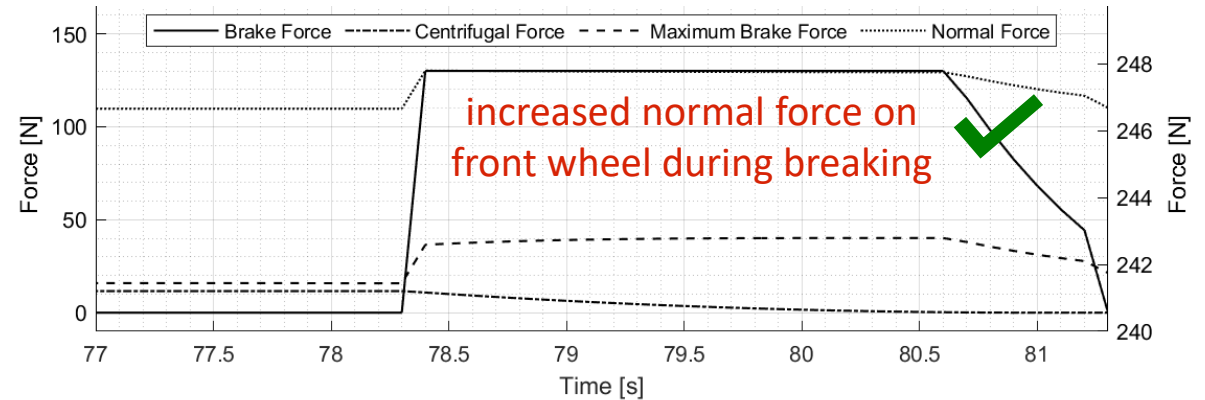


narrower curves/smaller curve radius

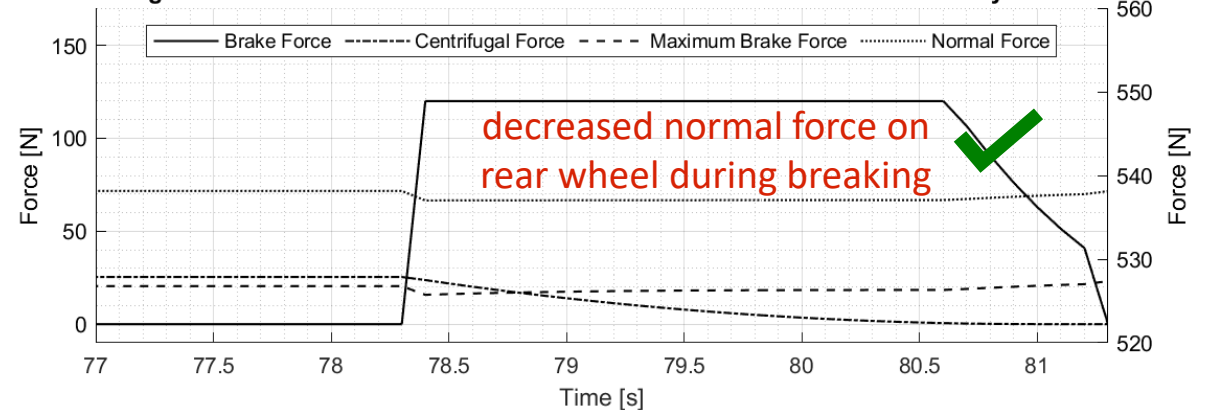
→ increased steering and tilt angle



Braking at a curve radius of 100 m and from a speed of 24 km/h



Braking Forces on the Rear Wheel at a Curve Radius of 100 m and from a Velocity of 24 km/h



→ decreasing centrifugal force leads to increase of maximum braking force



Conclusion and Future Work



Conclusion:

- Approach towards a holistic model of cycling dynamics to be used in standalone simulation of cycling
- Longitudinal, lateral and vertical dynamics as well as dynamic limitations are described as function of a propulsion force, trajectory and route properties
- Simulink implementation of achieved dynamics description
- Verification shows that model is capable of plausibly representing the required cycling dynamics

Future Work:

- Qualitative evaluation of the model → further literature research and experiments for determining parameters
- Evaluation of the dynamics model – especially in comparison to real cycling situations
- Extended consideration of vertical dynamics description
- Further optimisation and continuous development according to given requirements from the model environment or given use-cases



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Thank you for your Attention

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