Power grids: Small Signal Stability vs. Dynamical Parameters

Melvyn Tyloo melvyn.tyloo@gmail.com





Fonds national suisse Schweizerischer Nationalfonds Fondo nazionale svizzero Swiss National Science Foundation

The 11th International Conference on Smart Grids, Green Communications and IT Energy-aware Technologies ENERGY 2021 Special Track on "Modelling Dynamics of Power Grids" (MoDyPoG)

References

MT, Jacquod IEEE Control Systems Letters 5 (3), 929-934 (2020)

- MT, Pagnier, Jacquod Science Advances 5 (11):eaaw8359 (2019)
- MT, Jacquod Physical review E 101 (3), 032303 (2019) (=) (

Melvyn Tyloo (melvyn.tyloo@gmail.com)

Dr. Melvyn Tyloo

Melvyn obtained his master degree and PhD in Theoretical Physics at the Swiss Federal Institute of Technology in Lausanne (EPFL) respectively in 2016 and 2020. He is currently working as a postdoc researcher at the University of Geneva (UNIGE). His research focuses on complex network-coupled dynamical systems and the identification of their local/global vulnerabilities against external perturbations. He also recently developed methods for inferring coupling network from time-series and for locating line and node disturbances in diffusively coupled agents.



OrcID: 0000-0003-1761-4095 ResearcherID: T-7054-2017 Google Scholar ID: Melvyn Tyloo

Traditional transmission power grid



Traditional transmission power grid



Future transmission power grid



Traditional transmission power grid



Future transmission power grid



Motivation: Energy Transition



Swing equations in the lossless line approximation Voltage phase dynamics is given by

$$m_{i} \dot{\omega}_{i} + d_{i} \omega_{i} = P_{i} - \sum_{j} b_{ij} \sin(\theta_{i} - \theta_{j}), \quad i \in \text{Generators}, \quad (1)$$
$$d_{i} \omega_{i} = P_{i} - \sum_{j} b_{ij} \sin(\theta_{i} - \theta_{j}), \quad i \in \text{Loads}. \quad (2)$$

 b_{ij} : line capacity. m_i : inertia. d_i : damping. $\omega_i = \dot{\theta}_i$.

Bergen, Hill, "A structure preserving model for power system stability analysis," IEEE Trans. Power App. Syst., vol. PAS-100, no. 1, pp. 25–35, dan. 1981...=

Swing equations in the lossless line approximation: The common assumption on dynamical parameters

$$\gamma^{-1} d_i \dot{\omega}_i + d_i \omega_i = P_i - \sum_j b_{ij} \sin(\theta_i - \theta_j).$$

 $\begin{array}{l} b_{ij}: \mbox{ line capacity.} \\ m_i: \mbox{ inertia.} \\ d_i: \mbox{ damping.} \\ \omega_i = \dot{\theta}_i \,. \\ \mbox{ Usual assumptions that allow analytical treatment: inertia-to-damping constant ratio } \gamma^{-1} = m_i/d_i \,, \, \forall i \,. \end{array}$

Swing equations in the lossless line approximation: The common assumption on dynamical parameters

$$\gamma^{-1} d_i \dot{\omega}_i + d_i \omega_i = P_i - \sum_j b_{ij} \sin(\theta_i - \theta_j) .$$

 $\begin{array}{l} b_{ij}: \mbox{ line capacity.} \\ m_i: \mbox{ inertia.} \\ d_i: \mbox{ damping.} \\ \omega_i = \dot{\theta}_i \,. \\ \mbox{ Usual assumptions that allow analytical treatment: inertia-to-damping constant ratio $\gamma^{-1} = m_i/d_i$, $\forall i$.$ We also take this assumption... but eventually say something about realistic power networks!} \end{array}$

Quadratic performance metrics: H₂ norms → Quantify the amplitude of the transient response following a disturbance.



Robustness Assessment





Performance vs. Topology \rightarrow Generalized Kirchhoff indices Kf_n and resistance Centralities $C_n(k)$.

MT, Coletta, Jacquod *Physical review letters* **120** (8), 084101 (2018) MT, Pagnier, Jacquod *Science Advances* **5** (11):eaaw8359 (2019) MT, Jacquod *Physical review E* **101** (3), 032303 (2019)

Melvyn Tyloo (melvyn.tyloo@gmail.com)

ENERGY 2021

Swing equations in the lossless line approximation:

$$\gamma^{-1} d_i \ddot{\theta}_i + d_i \dot{\theta}_i = P_i - \sum_j b_{ij} \sin(\theta_i - \theta_j).$$

Linear response: Perturbation of the injected/consumed powers. - $P_i(t) = P_i^{(0)} + \delta P_i(t) \rightarrow \theta_i(t) = \theta_i^{(0)} + \delta \theta_i(t)$:

$$\gamma^{-1}\delta\ddot{\varphi}(t) + \delta\dot{\varphi}(t) = D^{-1/2}\delta P(t) - D^{-1/2}\mathbb{L}(\{\theta_i^{(0)}\})D^{-1/2}\delta\varphi(t) ,$$

where $\delta\varphi(t) = D^{1/2}\delta\theta(t) .$

Response to Perturbations: Linearization

Swing equations in the lossless line approximation:

$$\gamma^{-1} d_i \ddot{\theta}_i + d_i \dot{\theta}_i = P_i - \sum_j b_{ij} \sin(\theta_i - \theta_j).$$

Linear response: Perturbation of the injected/consumed powers.

-
$$P_i(t) = P_i^{(0)} + \delta P_i(t)
ightarrow heta_i(t) = heta_i^{(0)} + \delta heta_i(t)$$
:

$$\gamma^{-1} \,\delta \ddot{\varphi}(t) + \delta \dot{\varphi}(t) = D^{-1/2} \delta P(t) - D^{-1/2} \mathbb{L}(\{\theta_i^{(0)}\}) D^{-1/2} \delta \varphi(t) \;,$$

 $\mathbb{L}(\{\theta_i^{(0)}\})$: the weighted Laplacian matrix,

$$[D^{-1/2} \mathbb{L} D^{-1/2}]_{ij} = \begin{cases} -\frac{b_{ij}}{\sqrt{d_i d_j}} \cos(\theta_i^{(0)} - \theta_j^{(0)}), & i \neq j, \\ \frac{1}{d_i} \sum_k b_{ik} \cos(\theta_i^{(0)} - \theta_k^{(0)}), & i = j. \end{cases}$$

Response to Perturbations: Linearization

Linear response: Perturbation of the injected/consumed powers.

-
$$P_i(t) = P_i^{(0)} + \delta P_i(t)
ightarrow heta_i(t) = heta_i^{(0)} + \delta heta_i(t)$$
 :

$$\gamma^{-1}\,\delta\ddot{arphi}(t)+\delta\dot{arphi}(t)=D^{-1/2}\delta P(t)-D^{-1/2}\mathbb{L}(\{ heta_i^{(0)}\})D^{-1/2}\delta arphi(t)$$

Solution:

$$\delta\varphi_{i}(t) = \sum_{\alpha} \gamma e^{\frac{-\gamma - \Gamma_{\alpha}}{2}t} \int_{0}^{t} e^{\Gamma_{\alpha}t_{1}} \\ \times \int_{0}^{t_{1}} [D^{-1/2}\delta P(t_{2})]^{\top} u_{\alpha}^{D} e^{\frac{\gamma - \Gamma_{\alpha}}{2}t_{2}} \mathrm{d}t_{2} \mathrm{d}t_{1} \ u_{\alpha,i}^{D} , \qquad (3)$$

Time-correlated power fluctuations:

$$\langle \delta P_i
angle = 0$$
 , $\langle \delta P_i(t) \delta P_j(t')
angle = \delta_{ij} \delta P_0^2 \exp[-|t-t'|/ au_0]$.

Primary control effort:

$$\begin{aligned} \mathcal{P}(T) &= \lim_{T \to \infty} T^{-1} \, \int_0^T (\boldsymbol{\omega}^\top - \overline{\boldsymbol{\omega}}^\top) D(\boldsymbol{\omega} - \overline{\boldsymbol{\omega}}) \, \mathrm{d}t \,, \\ &= \lim_{T \to \infty} T^{-1} \, \int_0^T (\delta \boldsymbol{\varphi}^\top - \overline{\delta \boldsymbol{\varphi}}^\top) (\delta \boldsymbol{\varphi} - \overline{\delta \boldsymbol{\varphi}}) \, \mathrm{d}t \,. \end{aligned}$$

Linear system \rightarrow analytical solution!

∃ ▶ ∢

Primary control effort:

$$\overline{\mathcal{P}^{\infty}} = \sum_{\alpha \ge 2} \frac{\sum_{i \in \mathcal{N}_n} \delta \mathcal{P}_{0i}^2 u_{\alpha,i}^{D^2} d_i^{-1}}{\lambda_{\alpha}^D \tau_0 + 1 + \gamma^{-1} \tau_0^{-1}} ,$$

with λ_{α}^{D} the eigenvalue associated with the eigenvector \mathbf{u}_{α}^{D} of \mathbb{L}^{D} .

Primary Control Effort

Short noise correlation time: $\tau_0 \ll \gamma^{-1}, \lambda_{\alpha}^{D^{-1}}$

$$\overline{\mathcal{P}^{\infty}} = \tau_0 \sum_{i \in N_n} \delta P_{0i}^2 \left(1/m_i - 1/\sum_j m_j \right) \,.$$

No dependence on damping nor network connectivity! Long correlation time: $\tau_0 \gg \gamma^{-1}, \lambda_{\alpha}^{D^{-1}}$

$$\overline{\mathcal{P}^{\infty}} = \tau_0^{-1} \sum_{\alpha \ge 2} \frac{\sum_{i \in N_n} \delta P_{0i}^2 u_{\alpha,i}^{D^2} d_i^{-1}}{\lambda_{\alpha}^D} \ .$$

No dependence on inertia!

Primary Control Effort

Short noise correlation time: $\tau_0 \ll \gamma^{-1}, \lambda_{\alpha}^{D^{-1}}$

$$\overline{\mathcal{P}^{\infty}} = \tau_0 \sum_{i \in N_n} \delta P_{0i}^2 \left(1/m_i - 1/\sum_j m_j \right) \,.$$

No dependence on damping nor network connectivity! Long correlation time: $\tau_0 \gg \gamma^{-1}, \lambda_{\alpha}^{D^{-1}}$

$$\overline{\mathcal{P}^{\infty}} = \tau_0^{-1} \sum_{\alpha \ge 2} \frac{\sum_{i \in N_n} \delta \mathcal{P}_{0i}^2 u_{\alpha,i}^{D^2} d_i^{-1}}{\lambda_{\alpha}^D}$$

No dependence on inertia!

Realistic high-voltage power networks: $\lambda_{\alpha}^{D^{-1}} < 0.5s$ and $\gamma^{-1} \cong 2.5s$. Renewable power sources fluctuate on time scales of few seconds.

IEEE 118-Bus Test Case:



MT, Jacquod IEEE Control Systems Letters 5 (3), 929-934 (2020)

ENERGY 2021

Numerical Validation

PanTaGruEI:



MT, Jacquod IEEE Control Systems Letters 5 (3), 929-934 (2020)

ENERGY 2021

Description of realistic power networks

- Consider $D^{-1/2} \mathbb{L} D^{-1/2}$ instead of $M^{-1/2} \mathbb{L} M^{-1/2}$,
- Time-correlated noise instead of white-noise,
- \rightarrow Primary control effort for power networks with inhomogeneous dynamical parameters.
- Inertia does not impact much primary control effort.
- \rightarrow Focus on damping/control.

Melvyn Tyloo (melvyn.tyloo@gmail.com)