



Towards estimations of continuous cardiac output with impedance cardiography: a pilot study





Authors: Chao-Ting Liu, Po-Hsun Huang, Tzu-Chien Hsiao Presenter: Chao-Ting Liu, Institute of Biomedical Engineering National Chiao Tung University, Hsinchu, Taiwan R.O.C. Email address:dfr1507@gmail.com







Educational experience:

- 2013/09-2017/06: Department of Electronics Engineering, Chang Gung University
- 2017/07-now: Institute of Biomedical Engineering, College of Electrical and Computer Engineering, National Chiao Tung University

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2017 Certified LabVIEW Associate Developer (CLAD, 100-317-22466)





> Introduction

- 1.1 Background
 - Hemodynamics
 - Cardiopulmonary interactions
 - Impedance cardiography (ICG)
 - History from CO to SV measurement
- ■1.2 Motivation
- 1.3 Objective

> Material and Method

- 2.1 The block diagram of ICG system
 - Voltage controlled current source
 - Simulating signal
 - Amplitude demodulation
- 2.2 Experiment procedure
- 2.3 Signal processing

≻ Result

- Discussion
- Conclusion & Further work

Reference

Hemodynamics

- Hemodynamics is the study of blood flow and circulation between tissues and organs, the circulatory system can be divided into systemic circulation (Heart to Tissue) and pulmonary circulation (Heart to Lung).
 Tissue capillaries training
- Hemodynamic parameters
 - •Blood oxygen saturation (SpO2) by pulse Oximeter
 - Evaluate blood oxygen content
 - •Partial pressure of oxygen (PO2) by withdrawing blood
 - Evaluate gas exchange function of pulmonary
 - •Blood pressure (BP) by sphygmomanometer
 - The pressure exerted by blood on the vessel wall
 - Arteriopathy: atherosclerosis, hemangioma, aortic dissection
 - •Stroke volume (SV) by Impedance cardiography (ICG) and Doppler ultrasound (Non-invasive)
 - Evaluate cardiac contractility and cardiac regulation function
 - Cardiac output (CO) by Pulse induced contour cardiac output (PiCCO) and Pulmonary artery activation (PAC) (Invasiva)
 - Pulmonary artery catheter (PAC) (Invasive)
 - Evaluate cardiac pumping performance by long-term CO observation.



Cardiopulmonary interactions



Impedance cardiography (ICG)

During heart beating, the corresponding relationship between ECG and ICG, as well as the important characteristic points and intervals.





Activation of the atria

Activation of the ventricles AV node and ventricles fire

Recovery wave ventricles recharge

T wave



 $(Z=Z_0+\Delta Z_C+\Delta Z_R, Z_0=basic impedance; \Delta Z_C=impedance change caused by cardiac cycle; \Delta Z_R=impedance change caused by respiratory)$

Point	Description
B	Corresponding to the opening of the aortic
	valve.
С	(dZ/dt) _{max} : This point can reflect the
	maximum speed of impedance change,
	which is related to the maximum ejection
	speed of the heart.
X	Corresponding to the closure of the aortic
	valve.

Period	Description
Q-B	The time interval between Q wave and the
	opening of the aortic valve is called pre-
	ejection period (PEP).
B-X	The time interval between the opening and
	closing of the aortic valve is called left
	ventricular ejection time (T_{LVE}).

Berntson, G. G., et al., "Cardiovascular psychophysiology", 2017.

https://www.mdpi.com/1424-8220/20/7/2033/htm

History from CO to SV measurement

SV)
ve (
vasi
n-in
No

ultrasound

cardiometry

mpedance

Bio-

Invasive (CO)

Electrical

Doppler

 $SV = CSA \int v(t)dt$

 $SV = \overline{V}_{EPT} \left[\frac{(dZ/dt)_{max}}{Z_0} \right]^n T_{LVE}$

 $SV = \frac{L^3}{4.25} \frac{\delta}{Z_0} T_{LVE} \left(\frac{dZ}{dt}\right)_{max}$

 $\mathbf{SV} = \rho \frac{L^2}{Z_0^2} T_{LVE} \left(\frac{\mathrm{dZ}}{\mathrm{dt}}\right)_{max}$

 $CSA = \frac{\pi D^2}{4}$, D:aortic diameter.

n is an exponent which is <1.

• Huntsman (1983). Doppler ultrasound measures aortic diameter and aortic blood velocity. SV is determined by Blood velocity (v) and the cross-sectional area of the lumen (CSA).

• Feigenbaum (1967). propose ultrasound can be used to measure left ventricular stroke volume.

- Schmidt (2005). SV is estimated by the volume of electrically participating tissue (\overline{V}_{EPT}) derived from the body mass and height and aortic blood velocity during left ventricular ejection.
- Bernstein and Osyka (2001) proposed electrical cardiometry.
- **Bernstein** (1986) modified SV equation. ($\delta = \sqrt{(BMIp/24 \text{ kg m}^{-2})}$ where BMI_p = patient body mass index (kg m⁻²), 24 kg m⁻² = ideal BMI.)
- Kubicek (1974) estimate SV by using the maximum change of impedance and Left ventricular ejection time (T_{LVE}) . (ρ = static specific resistance of blood; L = the measured thoracic length between voltage sensing electrodes); Z_0 = base impedance; $(dZ/dt)_{max}$ = the maximum change of impedance.)
- Kedrov (1949) Firstly measuring the electrical impedance change.
 - Fegler (1954) proposed the thermodilution (TD) of CO determination.

• Hamilton (1927) used dye dilution method to calculate CO in humans.

• Stewart (1897) used Solution dilution method to obtain CO measurement for dogs.

• Fick (1870) defined CO measurement as estimating the amount of liters pumped by the heart in mins.





In the laboratory, I was exposed to the physiological signal of impedance cardiography (ICG), which can monitor cardiac output and condition of cardiac health, let me be curious if ICG can be used to understand the changes of breathing and heart pumping during exercise.

Growth process:

Motivation





> Hypothesis:

- 1. ICG is a suitable way to estimate SV and get the original signal.
- 2. The physiological phenomenon of respiration can be reflected on ICG signal.

> Objective:

- 1. Designing ICG measurement system and obtain ICG raw data.
- 2. Calculating the stroke volume during exercise by our systems.
- 3. Observe respiratory signal from ICG signal.

The block diagram of ICG system



Voltage controlled current source

Howland current pump circuit:



Figure.3. Howland current pump circuit

$$I_{\text{out}} = \frac{1}{R_{2b}} \frac{R_4}{R_3} \left(\frac{R_{2a} + R_2 \frac{R_3}{R_4}}{R_{2a} + R_1} V_{\text{in}+} - V_{\text{in}-} \right) + \frac{R_4 R_1 - R_2 R_3}{R_3 R_{2b} (R_1 + R_{2a})} V_{\text{out}}$$

Where R_2 is the sum of R_{2a} and R_{2b} . If the following relationship is assumed,

$$\frac{R_2}{R_1} = \frac{R_4}{R_3}$$

$$\frac{I_{\text{out}}}{V_{\text{in+}} - V_{\text{in-}}} = \frac{1}{R_{2b}} \frac{R_4}{R_3} = \frac{1}{R_{2b}} \frac{1 - \beta_{\text{fb}}}{\beta_{\text{fb}}}$$
Where $\beta_{fb} = \frac{R_3}{(R_3 + R_4)}$; and the circuit becomes a voltage to current converter with differential inputs.

Mahnam, A., Yazdanian, H., & Samani, M. M. (2016). Comprehensive study of Howland circuit with non-ideal components to design high performance current pumps. Measurement, 82, 94-104.



Simulating signal:



Load (1000 ohm):



Protection circuit :

- > The protection circuit is set with **diodes**.
- Based on the characteristics of diodes, if the signal flowing through the human body exceeds the set voltage, it will pass through the diode and lead into the ground.



Amplitude demodulation

Synchronous detector

By inputting the AM modulated signal and the AM carrier to the multiplier, the original signal and the the carrier and its harmonics can be obtained.





> Data Acquisition

■Ambu® Sleepmate RIPmate[™] Inductance Belts

- Biomedical Sensor Pad
- •NI USB-6210
- **•NI Elvis**

ICG Measurement Circuit (Power Supply:12V battery, Output Current:1.8mA)









(NCTU-REC-108-109F)









Procedure

(Except training stage, others are totally spontaneous breathing.)



Signal processing_ICG



Signal processing_respiratory signal





#Subject1



00





ICG & ECG signalEstimation of SV during exercise



Only measuring ICG



Simultaneous measuring ICG and ECG



When ICG and ECG signals are measured at the same time, the signals will affect each other.
We can deal with this problem by the T-wave ratio of ECG to the x-point of ICG.



#Subject1

> Estimation of SV during exercise:



The feature points of ICG can not be identified accurately.

- In ICG measurement during motion, the signal will be affected by motion artifact and respiratory, resulting in the influence of feature point discrimination.
- The traditional signal processing method of ICG is filter. The filter has the problem of phase shift.
- ➤ We think that other signal processing methods can deal with this problem, and improve the signal distortion caused by motion artifact and respiratory, so as to improve the accuracy of SV estimation.

Conclusion & Further work

- ➤ This study shows that the impedance variation and ICG may be detected by the modified circuit, and can further estimate the SV.
- ➢ In the past studies, it was also pointed out that there was a certain relationship between the heart beating process and the respiratory mechanism. We made empirical studies through the way of paced breathing and biking.
- However, the current measurement results in the process of motion are also affected by the influence of motion artifact and respiratory, resulting in the signal feature points can not be clearly identified in some cases.
- ➢ In future work, we hope to estimate SV more accurately during exercise by signal processing, such as Empirical Mode Decomposition (EMD).



Thanks for your attention

Q & A



- [1] Kubicek, W. G., et al., "Development and evaluation of an impedance cardiac output system", Aerospace Medicine, 37, 1208-1212, 1966.
- [2] Bernstein, D. P., "Continuous noninvasive real-time monitoring of stroke volume and cardiac output by thoracic electrical bioimpedance," Critical care medicine, 14(10), 898-901, 1986.
- [3] Lababidi, Z., et al., "The first derivative thoracic impedance cardiogram". Circulation, 41(4), 651-658, 1970.
- [4] Zhang, Y., et al., "Cardiac output monitoring by impedance cardiography during treadmill exercise", IEEE Transactions on Biomedical Engineering, (11), 1037-1042, 1986.
- [5] Shyu, L. Y., et al., "Portable impedance cardiography system for real-time noninvasive cardiac output measurement", Journal of Medical and Biological Engineering, 20(4), 193-202, 2000.
- [6] Yazdanian, H., et al., "Design and implementation of a portable impedance cardiography system for noninvasive stroke volume monitoring", Journal of Medical Signals and Sensors, 6(1), 47, 2016.
- [7] N. E. Huang et al., "The empirical mode decomposition and the Hilbert spectrum for nonlinear and non-stationary time series analysis", Proceedings of the Royal Society of London. Series A: Mathematical, Physical and Engineering Sciences, 454: 903–995, 1998.
- [8] Yeh, J. R., et al., "Complementary ensemble empirical mode decomposition: A novel noise enhanced data analysis method", Advances in Adaptive Data Analysis, 2(02), 135-156, 2010.
- [9] Chen, Y. C., et al., "Breathing pattern recognition of abdominal wall movement by using ensemble empirical mode decomposition", Advances in Adaptive Data Analysis, 6(01), 1450002, 2014.
- [10] A.S. Ross, et al., "Current source design for electrical impedance tomography", Physiological Measurement, 24(2), 509, 2003.



- [11] L. Constantinou, et al., "Highpower CMOS current driver with accurate transconductance for electrical impedance tomography", IEEE Transactions on Biomedical Circuits and Systems, 8(4), 575-583, 2014.
- [12] G. Cybulski, Ambulatory Impedance Cardiography, Springer, 2011.
- [13] Y. Mohamadou, et al., "Performance evaluation of wideband bio-impedance spectroscopy using constant voltage source and constant current source", Measurement Science and Technology, 23(10), 105703, 2012.
- [14] Lukaski, H. C., et al., "Validation of tetrapolar bioelectrical impedance method to assess human body composition", Journal of Applied Physiology, 60(4), 1327-1332, 1986.
- [15] Wang, F. T., et al., "Instantaneous respiratory estimation from thoracic impedance by empirical mode decomposition", Sensors, 15(7), 16372-16387, 2015.
- [16] Thome, F., et al., "Novel destructive-interference-envelope detector for high data rate ASK demodulation in wireless communication receivers", IEEE MTT-S International Microwave Symposium (pp. 1-4), 2015
- [17] Pellon, L. E., "A double Nyquist digital product detector for quadrature sampling",
- IEEE Transactions on Signal processing, 40(7), 1670-1681, 1992.
- [18] Yassa, F. F., & Noujaim, S. E., "Adaptive synchronous amplitude demodulation",
- In Twenty-Second Asilomar Conference on Signals, Systems and Computers (Vol. 1, pp. 107-111), 1988.
- [19] Costas, J. P., Synchronous communications. Proceedings of the IRE, 44(12), 1713-1718, 1956.
- [20] Brock, R. C., "Pulmonary valvulotomy for congenital pulmonary stenosis", British Medical Journal, 1(4562), 1121, 1948.



- [21] Siu, S. C., et al., "Bicuspid aortic valve disease", Journal of the American College of Cardiology, 55(25), 2789-2800, 2010.
- [22] Denniston, J. C., et al., "Measurement of cardiac output by electrical impedance at rest and during exercise", Journal of Applied Physiology, 40(1), 91-95, 1976.
- [23] Ganz, W., et al., "A new technique for measurement of cardiac output by thermodilution in man", The American Journal of Cardiology, 27(4), 392-396, 1971.
- [24] Ono, T., et al., "Validity of the adaptive filter for accurate measurement of cardiac output in impedance cardiography", The Tohoku Journal of Experimental Medicine, 202(3), 181-191, 2004.
- [25] Ernst, J. M., et al., "Impedance pneumography: Noise as signal in impedance cardiography", Psychophysiology, 36(3), 333-338, 1999
- [26] Yasuma, F., & Hayano, J. I., "Respiratory sinus arrhythmia: why does the heartbeat synchronize with respiratory rhythm?', Chest, 125(2), 683-690, 2004.
- [27] Chang, K. M., "Arrhythmia ECG noise reduction by ensemble empirical mode decomposition (EEMD)", Sensors, 10(6), 6063-6080, 2010.
- [28] Chen, Y. C. & Hsiao, T. C., "Instantaneous phase difference (IPD) analysis between thoracic and abdominal movement signals based on complementary ensemble empirical mode decomposition", Biomedical Engineering Online, 15(1), 112, 2016.
- [29] Cybulski, G., "Ambulatory impedance cardiography. In: Ambulatory Impedance Cardiography", Springer, Berlin, Heidelberg, p. 39-56, 2011.
- [30] Berntson, G. G., et al., "Cardiovascular psychophysiology", 2017.
- [31] G. A. Roth et al., "Global, regional, and national burden of cardiovascular diseases for 10 causes, 1990 to 2015," Journal of the American College of Cardiology, 70(1), pp. 1-25, 2017.

• [32] M. A. Branthwaite and R. D. Bradley, "Measurement of cardiac output by thermal dilution in man," Journal of Applied Physiology, 24(3), pp.434-438, 1968.

- [33] J. B. Mark et al., "Continuous noninvasive monitoring of cardiac output with esophageal Doppler ultrasound during cardiac surgery," Anesthesia and analgesia, 65(10), pp. 1013-1020, 1986.
- [34] G. Cybulski, "Ambulatory impedance cardiography The Systems and their applications," Springer, Berlin, Heidelberg, pp. 39-56, 2011.
- [35] Malmivuo, J. and Plonsey, R., "Principles and applications of bioelectric and biomagnetic fields", chapter, 15, 12, 1995.
- [36] D. P. Bernstein and H. J. M. Lemmens, "Stroke volume equation for impedance cardiography," Medical and Biological Engineering and Computing, 43(4), pp. 443-450, 2005.
- [37] Kubicek, W. G., et al D., "The Minnesota impedance cardiograph-theory and applications. Bio-Medical Engineering", 9(9), 410-416, 1974.
- [38] Bogert, L. W. J., et al., "Pulse contour cardiac output derived from non-invasive arterial pressure in cardiovascular disease. Anaesthesia", 65(11), 1119-1125, 2010.
- [39] Fegler, G., "Measurement of cardiac output in anaesthetized animals by a thermo-dilution method. Quarterly Journal of Experimental Physiology and Cognate Medical Sciences: Translation and Integration", 39(3), 153-164, 1954.
- [40] Huntsman, L. L., et al., "Noninvasive Doppler determination of cardiac output in man", Clinical validation. Circulation, 67(3), 593-602, 1983.
- [41] Schmidt, C., et al., "Comparison of electrical velocimetry and transoesophageal Doppler echocardiography for measuring stroke volume and cardiac output", British Journal of Anaesthesia, 95(5), 603-610, 2005.

Reference



Reference

- [43] T. E. Kirby, "The CO2 rebreathing technique for determination of cardiac output," J. Cardiac Rehab., vol. 5, pp. 97-101 and 132-138, 1985.
- [44] Phillips, C. L., Parr, J. M., & Riskin, E. A., "Signals, systems, and transforms", Upper Saddle River: Prentice Hall, 2003.
- [45] Visscher, M. B., & Johnson, J. A., "The Fick principle: analysis of potential errors in its conventional application", Journal of Applied Physiology, 5(10), 635-638, 1953.
- [46] Stewart, G. N., "Researches on the circulation time and on the influences which affect it", The Journal of physiology, 22(3), 159, 1897.
- [47] W. F. Hamilton., et al., "Studies on the circulation IV", Ibid., 99, pp. 534-551, 1932.
- [48] Shepherd, J. T., Bowers, D., & Wood, E. H., "Measurement of cardiac output in man by injection of dye at a constant rate into the right ventricle or pulmonary artery", Journal of applied physiology, 7(6), 629-638, 1955.
- [49] Noordergraaf, A., Circulatory system dynamics (Vol. 1). Elsevier, 2012.
- [50] http://sphweb.bumc.bu.edu/otlt /MPH-Modules/PH/PH709_Heart/PH709_Heart2.html