





## Polymer Photonic Crystal Membrane for Human Body Thermoregulation

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#### Presenter



Mohamed Boutghatin, PhD student at the IEMN laboratory in France. The supervisors of my thesis work are: Yan Pennec and Vincent Thomy. The subject of my thesis is dealing with a new generation of textiles capable of regulating the temperature of the skin in order to maintain thermal comfort. The study is based on analytical calculations and numerical simulation codes using proven calculation methods such as the Finite Element Method (FEM). The theoretical study is followed by the fabrication of membranes in a clean room using high-performance nanotechnology methods and equipment.

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#### Context



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#### Context

The human body is assimilated to a black body. The emissivity of the human skin at 34 °C is given by Planck's

law:  

$$L^{0} = \frac{2hc^{2}}{\lambda^{5}} \cdot \frac{1}{e^{hc}/(\lambda kT) - 1}$$
 en W.m<sup>-3</sup>.sr<sup>-1</sup>

Normal emissivity in the range [5-30 µm]



- More than 50 % of radiation is emitted in the midinfrared range [5-15  $\mu$ m].
- Human skin at 34 °C emits a maximum of radiations at the wavelenght 9.5 μm.

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## Objective



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## Outline

|        | Geometry and model                              |
|--------|-------------------------------------------------|
|        |                                                 |
|        | Optical properties of polyethylene (PE) polymer |
|        |                                                 |
|        | ) Thermal balance                               |
|        |                                                 |
|        | Conclusions and futur work                      |
| $\sum$ | Conclusions and futur work                      |







### Geometry



Polymer membrane under human body radiation from the skin 3D view of the polymer membrane of thickness **h**, drilled with a triangular array of air holes with period **P** and diameter **D**. In-plane view of the elementary unit cell

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#### Model



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#### **Polymer membrane**

• Polyethylene (PE)



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#### **Structured membrane**



Appearance of reflection peaks between 5 and 7  $\mu$ m related to the structuration of the membrane







## **Origin of the peaks**

#### Snapshots of the modulus of the electric field for the three peaks of reflection A, **B** and **C**.



Symmetric mode with respect to the mid-plane of the membrane



Guided modes inside the membrane

Mode confined in the air hole







#### **Effect of geometry**

Variation of **h**, **D**, **P** according to a scaling factor  $\alpha$ 



| Scaling factor $\alpha_i$   | Period P (µm) | Diameter D (µm) | Thickness <i>h</i> (µm) |
|-----------------------------|---------------|-----------------|-------------------------|
| $\alpha_I = 1.0$            | 7.0           | 5.5             | 4.0                     |
| $\alpha_3 = 1.28$           | 9             | 7.1             | 5.1                     |
| <i>α</i> <sub>5</sub> =1.56 | 11.0          | 8.6             | 6.3                     |
| <i>α</i> <sub>7</sub> =1.84 | 13            | 10.2            | 7.4                     |
| $\alpha_9 = 2.12$           | 15.0          | 11.8            | 8.6                     |

Increasing the size of the geometrical parameters leads to the shift of the three reflective features A, B and C, towards higher wavelengths



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# Efficiency coefficient associated to R, T and A

$$\eta = \frac{\int_{\lambda_{\min}}^{\lambda_{\max}} E_{\lambda} \cdot \chi_{\lambda} \cdot d\lambda}{\int_{\lambda_{\min}}^{\lambda_{\max}} E_{\lambda} \cdot d\lambda} \text{ where:} \quad \cdot \quad \chi_{\lambda} \text{ is R, T or A in the range } [\lambda_{\min} - \lambda_{\max}] = [5-15 \,\mu\text{m}].$$



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#### **Thermal balance**



Assaf S., Boutghatin M. et al, Scientific reports, 2020

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#### Conductive heat flux

**Fourier's law**  $q_{cond} = k_{air} \frac{T_S - T_1}{d}$ 

#### • Convective heat flux

**Newton's law**  $q_{conv} = h_c(T_2 - T_a)$ 

• Radiative heat flux

#### Stephan-Boltzmann law

$$q_{rad,s} = \varepsilon_s \sigma T_s^4$$
$$q_{rad,a} = \varepsilon_a \sigma T_a^4$$
$$q_{rad,mi} = \varepsilon_m \cdot \sigma T_1^4$$
$$q_{rad,mo} = \varepsilon_m \cdot \sigma T_2^4$$

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Boutghatin M. et al, Nanomaterials, 2020







#### **Thermal balance**

#### **Resolution of the thermal equations**



- Due to very small thickness of our membrane, the temperature  $T_1 = T_2$ .
- For  $\alpha_9(P = 15 \ \mu m, D = 11.8 \ \mu m, h = 8.6 \ \mu m)$ , T<sub>a</sub> =

25.5 °C when the skin is covered by a non structured membrane, however  $T_a = 25$  °C when the same membrane is structured.

Room temperature  $(T_a)$  to achieve the thermal comfort  $(T_s = 34^{\circ}C)$ as a function of geometrical parameters of non structured membrane and structured one. Université







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| Geometry and model                              |  |
|-------------------------------------------------|--|
|                                                 |  |
| Optical properties of polyethylene (PE) polymer |  |
| Thermal balance                                 |  |
|                                                 |  |
| Conclusions and futur work                      |  |







#### Conclusions

- The structuration parameters of a PE membrane can modulate the optical coefficient in the mid-infrared.
- To maintain the thermal comfort, the PE photonic crystal membrane acts as a modulator under thermal radiation emitted from the human body.
- Compared to a non structured PE membrane, the structured one maintains the thermal comfort with a lower ambient temperature of 0.5 °C.
- The presence of micro-holes enables air permeability and can promote water-wicking

#### **Future work**

## Fabrication full PE membranes to compare the measured spectra with the simulation





- Develop a technical method for structuring a PE membrane.
- We seek to study photonic membranes based on active polymer, sensitive to ambient temperature and humidity.









